

Thermal Network Analysis with TNSolver

Steady Conduction - The Composite Wall Problem

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Outline

Heat Transfer Analysis using Thermal Networks

- ▶ Heat Transfer Math Model
 - └ Steady, plane wall conduction with convection
 - └ Control volumes and the integral form
- ▶ TNSolver User Guide
- ▶ Composite Wall Problem

Heat Transfer

Math Model

Conduction, Convection and Radiation

Help! The barn is on fire.

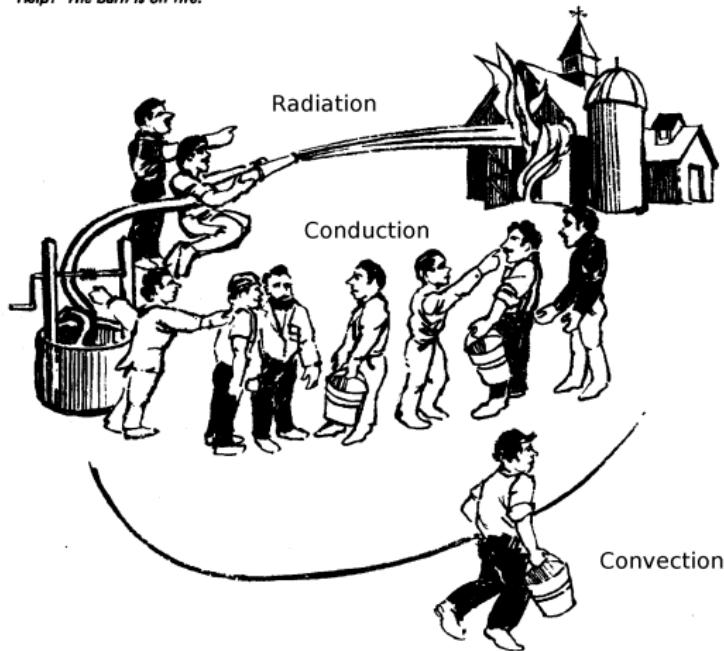


Figure borrowed from [LL12].

Heat Transfer Analysis

Math Model

Answering design questions about thermal energy and temperature

- ▶ Hand calculation - back-of-the-envelope
 - └ On the order of 1-10 equations
- ▶ Thermal network or lumped parameter approach
 - └ On the order of 10-1,000 equations
- ▶ Continuum approach - solid model/mesh generation
 - └ On the order of 1,000-1,000,000 equations
 - └ Finite Volume Method (FVM)
 - └ Finite Element Method (FEM)

See Section 1.5, page 38, in [BLID11]

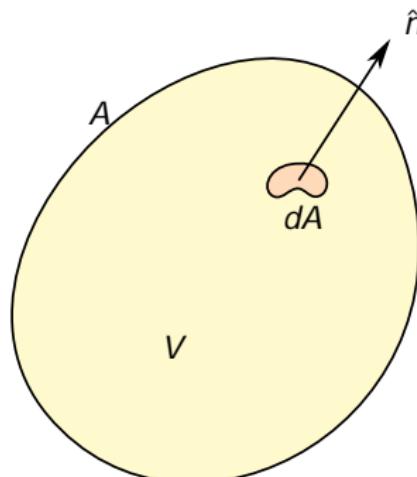
The Control Volume Concept

Math Model

$$\sum \text{Energy In} - \sum \text{Energy Out} =$$

Energy Stored, Generated and/or Consumed

Heat (transfer) is thermal energy transfer due to a temperature difference



Integral Form of Steady Heat Conduction

Math Model

The steady conduction equation, in Cartesian tensor integral form, is:

$$\int_A q_i n_i \, dA = \iint_V \dot{q} \, dV$$

where \dot{q} is a volumetric source and Fourier's Law of Heat Conduction provides a constitutive model for the heat flux as a function of temperature gradient:

$$q_i = -k \frac{\partial T}{\partial x_i}$$

where k is the isotropic thermal conductivity.

Convection

Math Model

Convection heat transfer from the surface of the control volume is modeled by:

$$\int_{\Gamma_c} q_i n_i dA = \int_{\Gamma_c} h(T_s - T_c) dA, \text{ where } \begin{cases} T_s > T_c, & \text{cooling} \\ T_s < T_c, & \text{heating} \end{cases}$$

The convection coefficient, $h(x_i, t, T_s, T_c)$, is usually a function of position, time, surface temperature, T_s , free stream or bulk temperature, T_c , and other parameters. The value of the coefficient is often evaluated using a correlation.

Introducing TNSolver

TNSolver User Guide

- ▶ Thermal Network Solver - TNSolver
- ▶ MATLAB/Octave program
 - ▷ GNU Octave is an open source clone of MATLAB
- ▶ Thermal model is described in a text input file
 - ▷ For example: edit using notepad on Windows
- ▶ Simulation results are both returned from the function and written to text output files for post-processing

Thermal Network Terminology

TNSolver User Guide

- ▶ Time dependency
 - | Steady state or transient
 - | Initial condition is required for transient
- ▶ Geometry
 - | Control Volume - volume, $V = \int_V dV$
 - | Node: ●, $T_{\text{node}} = \int_V T(x_i) dV$
 - | Control Volume Surface - area, $A = \int_A dA$
 - | Surface Node: ○, $T_{\text{surface node}} = \int_A T(x_i) dA$
- ▶ Material properties
- ▶ Conductors
 - | Conduction
 - | Convection
 - | Radiation
- ▶ Boundary conditions
 - | Boundary node: ▲
- ▶ Sources/sinks

TNSolver Input Example of Text Input File

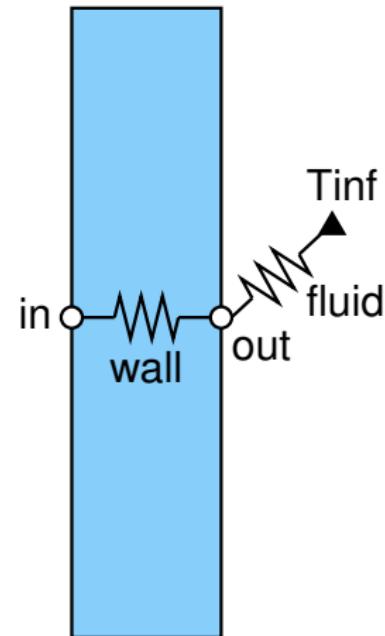
TNSolver User Guide

```
! Simple Wall Model

Begin Solution Parameters
  type = steady
End Solution Parameters

Begin Conductors
  wall conduction in out 2.3 1.2 1.0 ! k L A
  fluid convection out Tinf 2.3 1.0 ! h A
End Conductors

Begin Boundary Conditions
  fixed_T 21.0 in ! Inner wall T
  fixed_T 5.0 Tinf ! Fluid T
End Boundary Conditions
```



! begins a comment (MATLAB uses %)

Solution Parameters

TNSolver User Guide

```
Begin Solution Parameters

type  = steady ! <steady|transient>
units = SI        ! <SI|US>

End Solution Parameters
```

Conduction: Cartesian (The Plane Wall)

TNSolver User Guide

The rate of heat transfer, Q_{ij} , due to conduction, between the two temperatures T_i and T_j , separated by a distance L and area A , is:

$$Q_{ij} = \frac{kA}{L} (T_i - T_j)$$

The heat flux, q_{ij} , is:

$$q_{ij} = \frac{Q_{ij}}{A} = \frac{k}{L} (T_i - T_j)$$

Begin Conductors

```
! label type      node i node j parameters
name conduction  label  label    x.x x.x x.x ! k L A
```

End Conductors

Convection Conductor

TNSolver User Guide

The rate of heat transfer due to convection is:

$$Q_{ij} = hA(T_i - T_j)$$

```
Begin Conductors
```

```
! label type      node i node j  parameters
name convection  label  label   x.x x.x ! h A
```

```
End Conductors
```

Specified Surface Temperature Boundary Condition

TNSolver User Guide

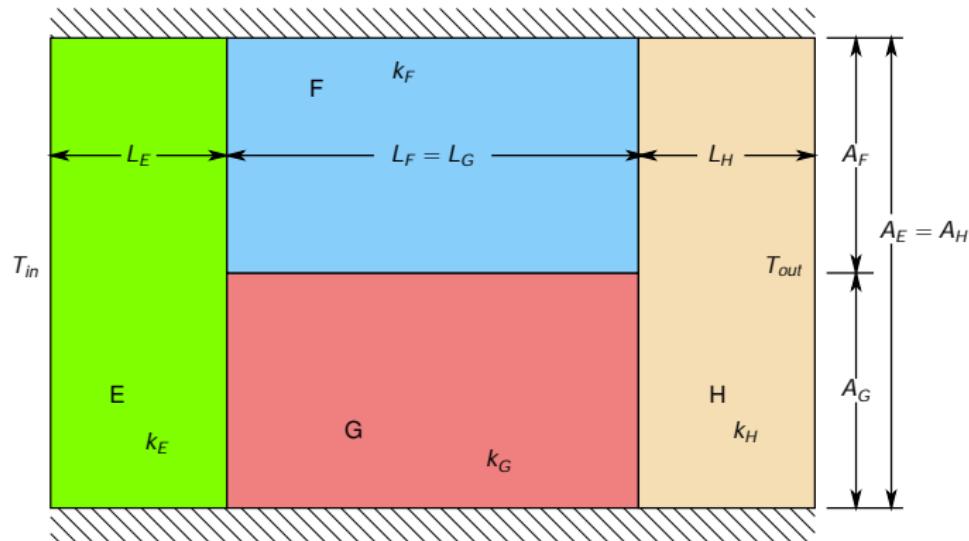
The surface node temperature, T_b is specified:

```
Begin Boundary Conditions
! type      parameter(s)    node(s)
fixed_T    T_b              label
End Boundary Conditions
```

Description of the Composite Wall Problem

Composite Wall Model

Consider a composite wall:



See Figure 3.3, on page 117, in [BLID11].

Model Parameters

Composite Wall Model

The inner wall temperature $T_{in} = 1$

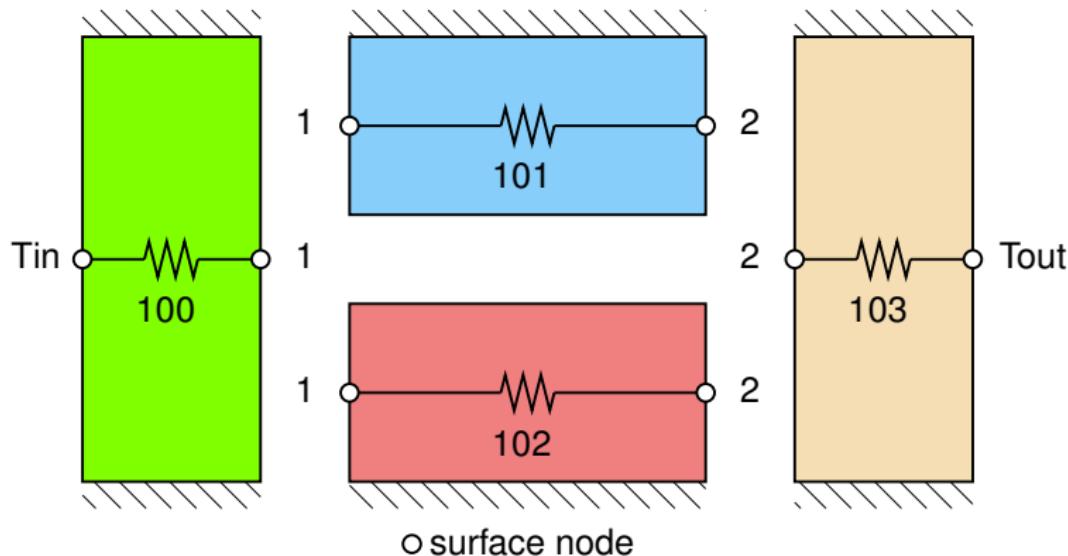
The outer wall temperature $T_{out} = 0$

Region	Conductivity, k	Length, L	Area, A
E	1.0	1.0	2.0
F	2.0	2.0	1.0
G	$0.001 \leq k_G \leq 2.0$	2.0	1.0
H	3.0	1.0	2.0

First Approach

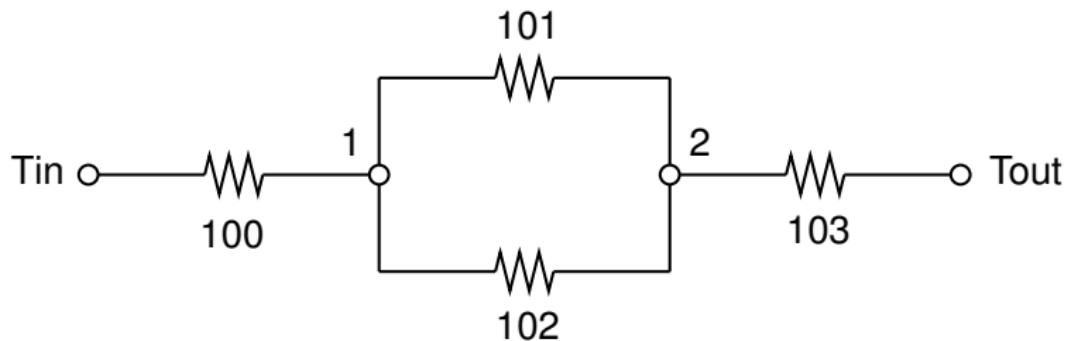
Composite Wall Model 1

There are four control volumes:



Network Diagram

Composite Wall Model 1



Compare with Figure 3.3 (a), on page 117, in [BLID11].

TNSolver Input File for $k_G = 2.0$

Composite Wall Model 1

```
!  Composite wall model: Approach 1 series-parallel

Begin Solution Parameters

type  = steady

End Solution Parameters

Begin Conductors

! label type      node 1  node 2  parameters
 100  conduction  Tin     1       1.0  1.0  2.0 ! k_E L_E A_E
 101  conduction  1       2       2.0  2.0  1.0 ! k_F L_F A_F
 102  conduction  1       2       2.0  2.0  1.0 ! k_G L_G A_G
 103  conduction  2       Tout   3.0   1.0  2.0 ! k_H L_H A_H

End Conductors

Begin Boundary Conditions

! type      parameter(s)    node(s)
fixed_T    1.0            Tin      ! inner wall temperature
fixed_T    0.0            Tout    ! outer wall temperature

End Boundary Conditions
```

TNSolver Output for $k_G = 2.0$

Composite Wall Model 1

Nodes

Label	Material	Volume (m ³)	Temperature (C)
Tin	N/A	0	1
1	N/A	0	0.571429
2	N/A	0	0.142857
Tout	N/A	0	0

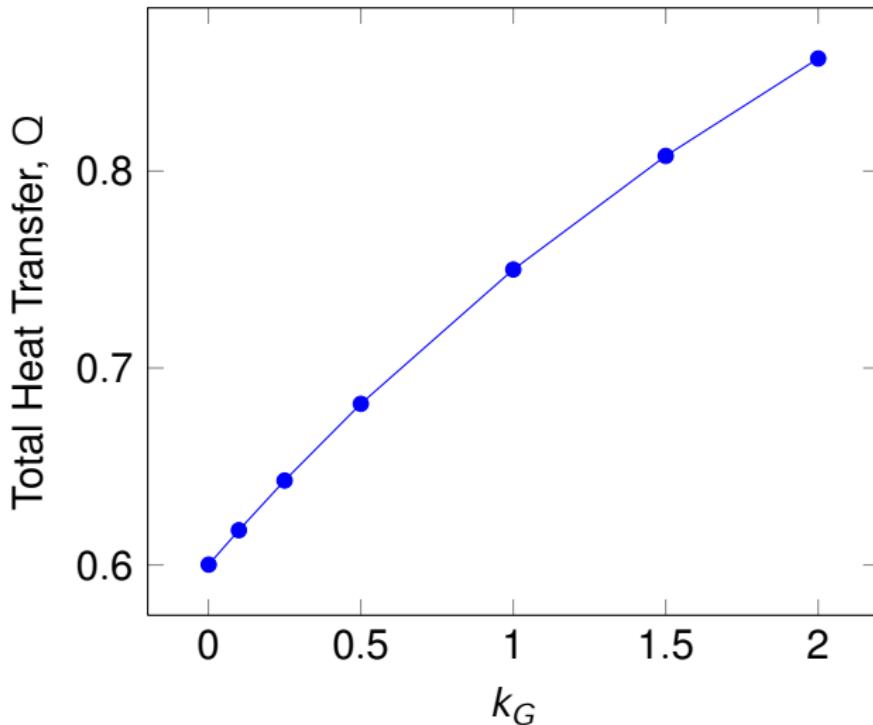
Conductors

Label	Type	Node i	Node j	Q_{ij} (W)
100	conduction	Tin	1	0.857143
101	conduction	1	2	0.428571
102	conduction	1	2	0.428571
103	conduction	2	Tout	0.857143

Total Heat Transfer over the Range of k_G

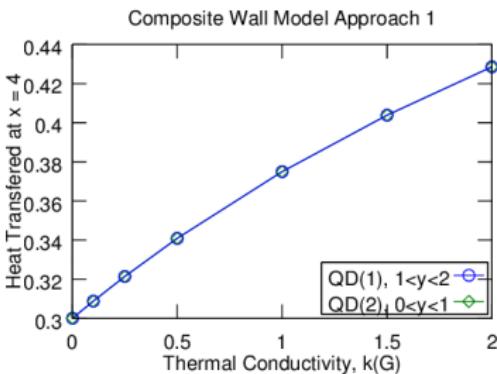
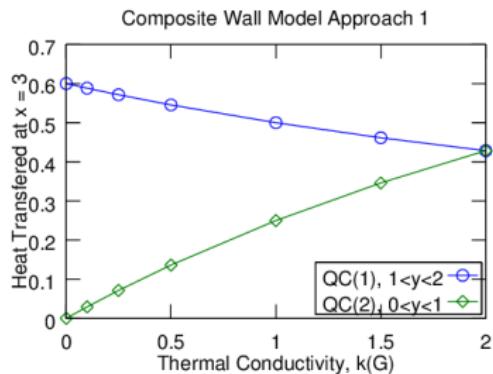
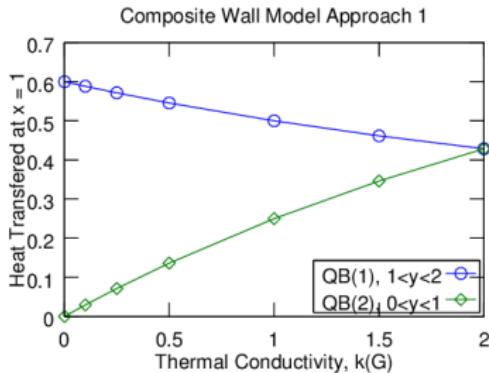
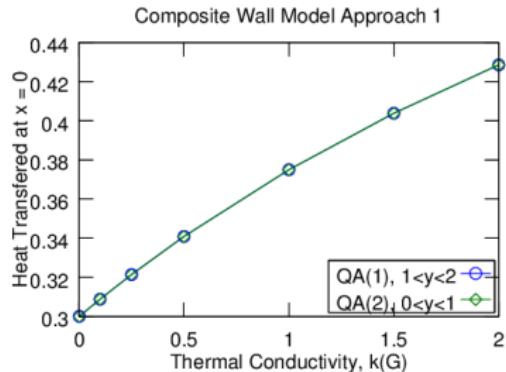
Composite Wall Model 1

Composite Wall, First Approach



Total Heat Transfer at Region Interfaces

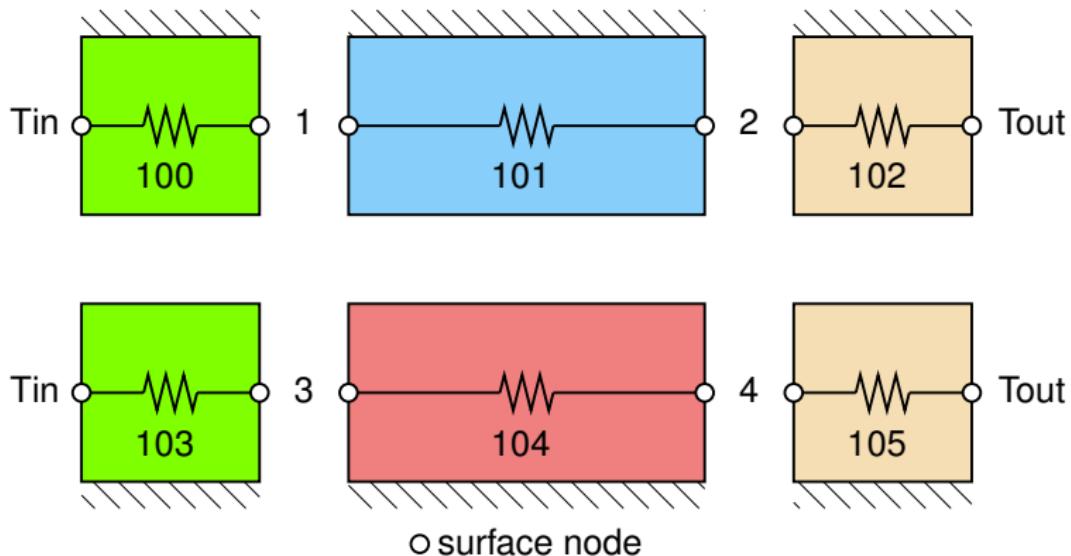
Composite Wall Model 1



Second Approach

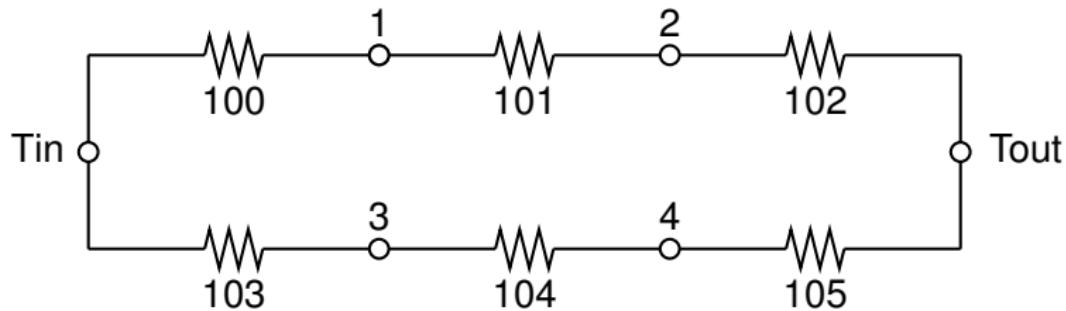
Composite Wall Model 2

There are six control volumes:



Network Diagram

Composite Wall Model 2



Compare with Figure 3.3 (b), on page 117, in [BLID11].

TNSolver Input File for $k_G = 2.0$

Composite Wall Model 2

```
! Composite wall model: Approach 2 - parallel conductors

Begin Solution Parameters

  type = steady

End Solution Parameters

Begin Conductors

! label  type      node 1  node 2  parameters
  100  conduction  Tin     1       1.0, 1.0, 1.0 ! k_E L_E A_E
  101  conduction  1       2       2.0, 2.0, 1.0 ! k_F L_F A_F
  102  conduction  2       Tout    3.0, 1.0, 1.0 ! k_H L_H A_H
  103  conduction  Tin     3       1.0, 1.0, 1.0 ! k_E L_E A_E
  104  conduction  3       4       2.0, 2.0, 1.0 ! k_G L_G A_G
  105  conduction  4       Tin    3.0, 1.0, 1.0 ! k_H L_H A_H

End Conductors

Begin Boundary Conditions

! type      parameter(s)  node(s)
  fixed_T    1.0          Tin     ! inner wall temperature
  fixed_T    0.0          Tout    ! outer wall temperature

End Boundary Conditions
```

TNSolver Output for $k_G = 2.0$

Composite Wall Model 2

Nodes

Label	Material	Volume (m ³)	Temperature (C)
T1	N/A	0	1
1	N/A	0	0.571429
2	N/A	0	0.142857
T2	N/A	0	0
3	N/A	0	0.571429
4	N/A	0	0.142857

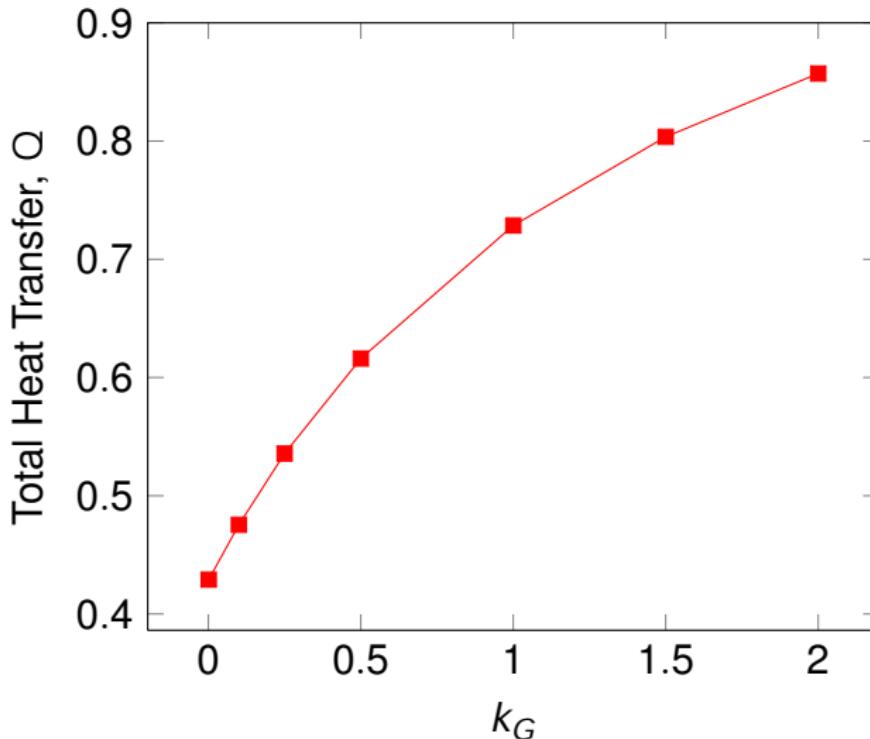
Conductors

Label	Type	Node i	Node j	Q_{ij} (W)
100	conduction	T1	1	0.428571
101	conduction	1	2	0.428571
102	conduction	2	T2	0.428571
103	conduction	T1	3	0.428571
104	conduction	3	4	0.428571
105	conduction	4	T2	0.428571

Total Heat Transfer over the Range of k_G

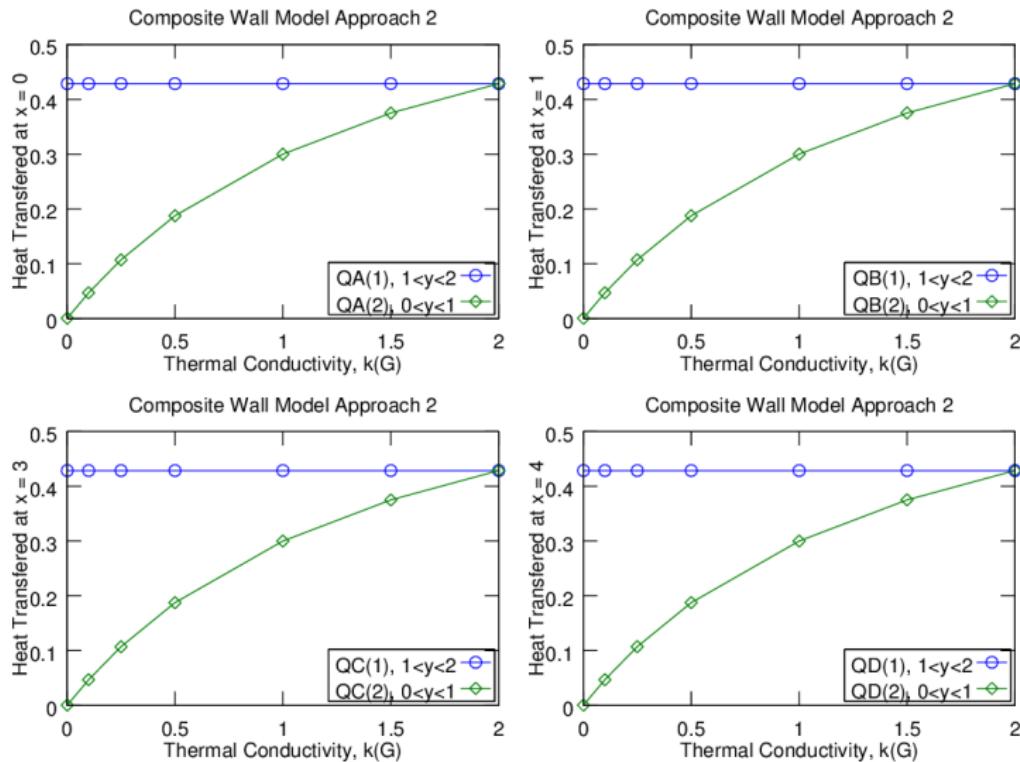
Composite Wall Model 2

Composite Wall, Second Approach



Total Heat Transfer at Region Interfaces

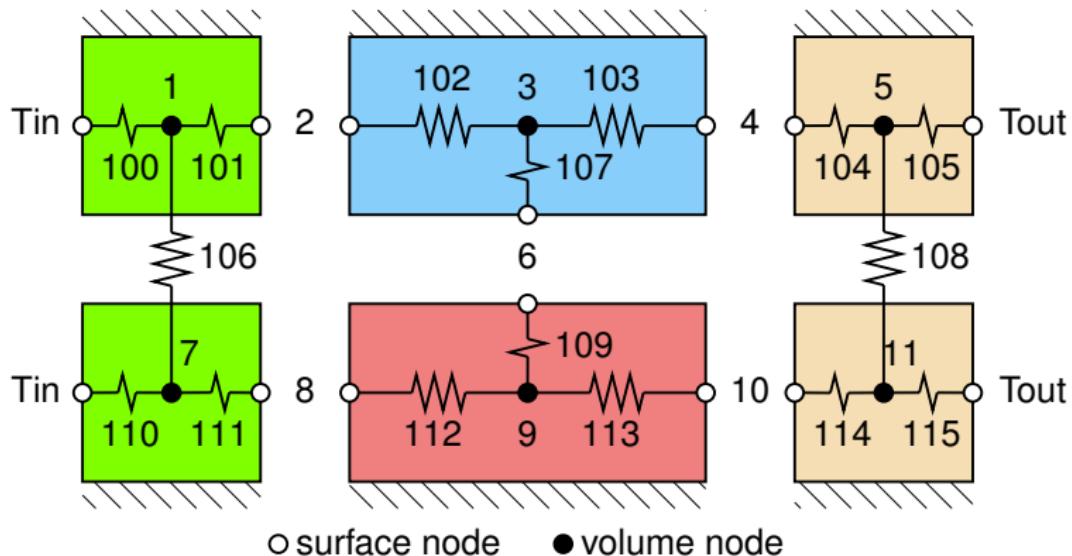
Composite Wall Model 2



Third Approach

Composite Wall Model 3

There are six control volumes:



TNSolver Input File for $k_G = 2.0$

Composite Wall Model 3

```
!  Composite wall model: Approach 3

Begin Solution Parameters

type  = steady

End Solution Parameters

Begin Conductors

! label type      node 1  node 2  parameters
 100 conduction Tin     1       1.0, 0.5, 1.0 ! k_E L_E A_E/2
 101 conduction 1      2       1.0, 0.5, 1.0 ! k_E L_E A_E/2
 102 conduction 2      3       2.0, 1.0, 1.0 ! k_F L_F A_F
 103 conduction 3      4       2.0, 1.0, 1.0 ! k_F L_F A_F
 104 conduction 4      5       3.0, 0.5, 1.0 ! k_H L_H A_H/2
 105 conduction 5      Tout   3.0, 0.5, 1.0 ! k_H L_H A_H/2

 106 conduction 1      7       1.0, 1.0, 1.0 ! k_E
 107 conduction 3      6       2.0, 0.5, 2.0 ! k_F
 108 conduction 5      11    3.0, 1.0, 1.0 ! k_H
 109 conduction 6      9       2.0, 0.5, 2.0 ! k_G

 110 conduction Tin     7       1.0, 0.5, 1.0 ! k_E L_E A_E/2
 111 conduction 7      8       1.0, 0.5, 1.0 ! k_E L_E A_E/2
 112 conduction 8      9       2.0, 1.0, 1.0 ! k_G L_G A_G
 113 conduction 9      10    2.0, 1.0, 1.0 ! k_G L_G A_G
 114 conduction 10    11    3.0, 0.5, 1.0 ! k_H L_H A_H/2
 115 conduction 11    Tout   3.0, 0.5, 1.0 ! k_H L_H A_H/2

End Conductors

Begin Boundary Conditions

! type      parameter(s)  node(s)
fixed_T    1.0          Tin     ! inner wall temperature
fixed_T    0.0          Tout   ! outer wall temperature

End Boundary Conditions
```

TNSolver Output for $k_G = 2.0$

Composite Wall Model 3

Nodes

Label	Material	Volume (m^3)	Temperature (C)
Tin	N/A	0	1
1	N/A	0	0.785714
2	N/A	0	0.571429
3	N/A	0	0.357143
4	N/A	0	0.142857
5	N/A	0	0.0714286
Tout	N/A	0	-1.13687e-013
7	N/A	0	0.785714
6	N/A	0	0.357143
11	N/A	0	0.0714286
9	N/A	0	0.357143
8	N/A	0	0.571429
10	N/A	0	0.142857

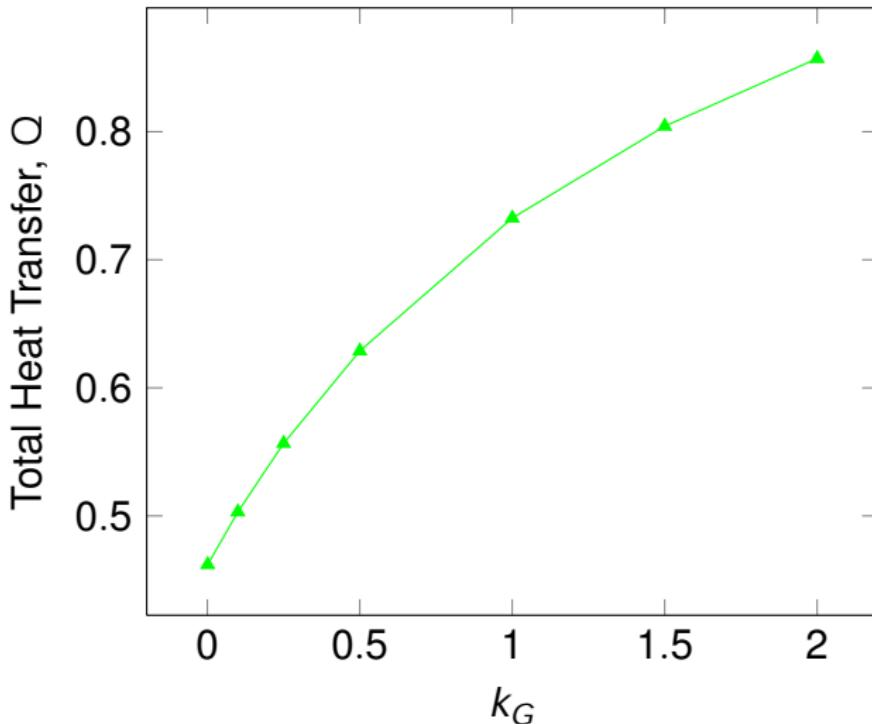
Conductors

Label	Type	Node i	Node j	Q_{ij} (W)
100	conduction	Tin	1	0.428571
101	conduction	1	2	0.428571
102	conduction	2	3	0.428571
103	conduction	3	4	0.428571
104	conduction	4	5	0.428571
105	conduction	5	Tout	0.428571
106	conduction	1	7	-5.68434e-014
107	conduction	3	6	0
108	conduction	5	11	-3.41061e-013
109	conduction	6	9	-4.54747e-013
110	conduction	Tin	7	0.428571
111	conduction	7	8	0.428571
112	conduction	8	9	0.428571
113	conduction	9	10	0.428571
114	conduction	10	11	0.428571
115	conduction	11	Tout	0.428571

Total Heat Transfer over the Range of k_G

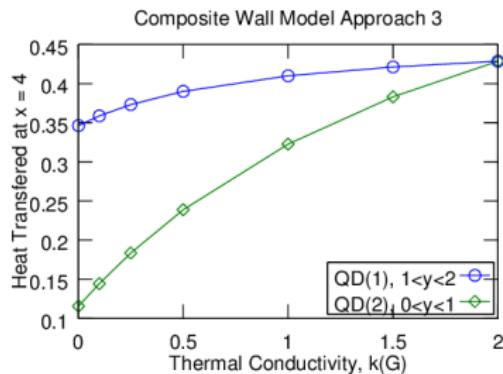
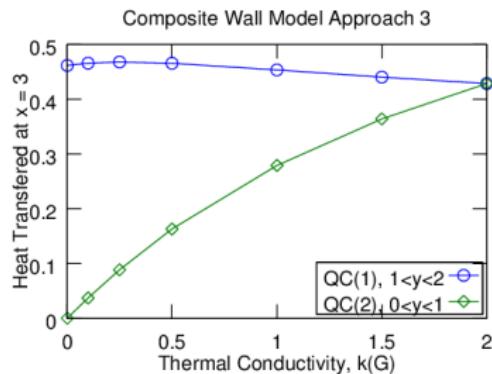
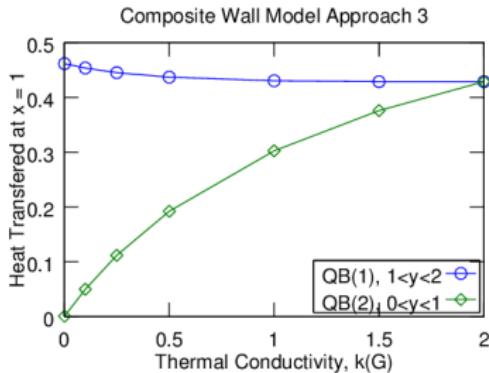
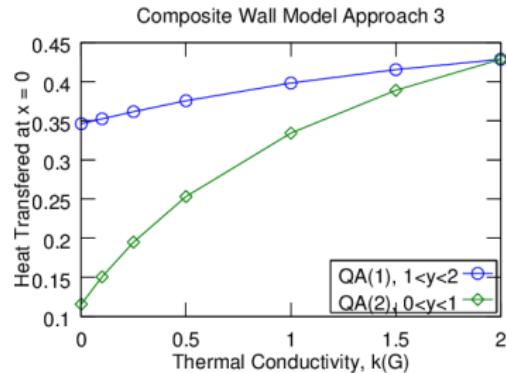
Composite Wall Model 3

Composite Wall, Third Approach



Total Heat Transfer at Region Interfaces

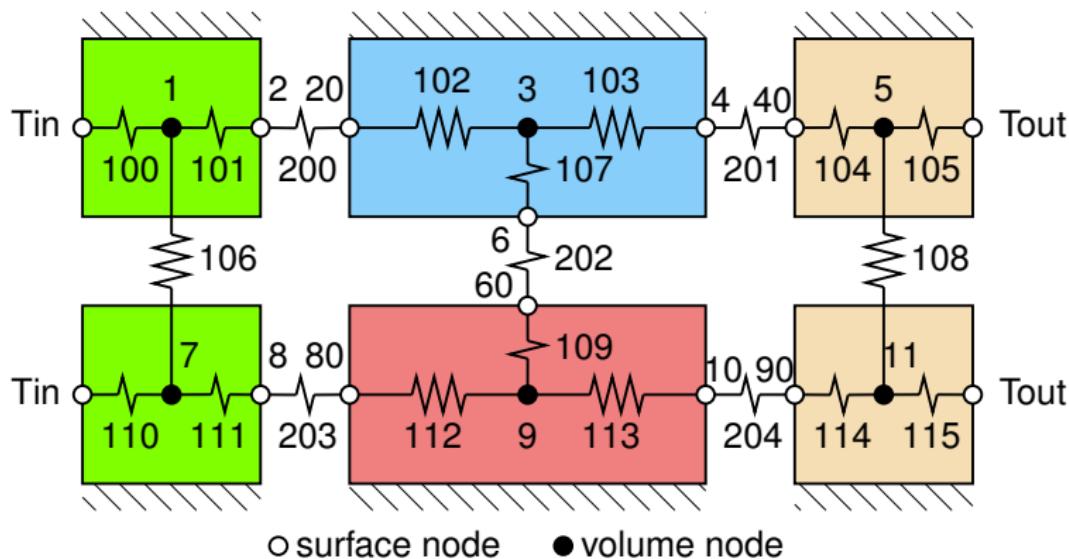
Composite Wall Model 3



Including Contact Resistance

Composite Wall Model 3 with Contact Resistance

There are six control volumes:



Contact resistance between the regions is $h = 0.10$

TNSolver Input File for $k_G = 2.0$

Composite Wall Model 3 with Contact Resistance

```
! Composite wall model: Approach 3 with Contact Resistance

Begin Solution Parameters

type = steady
units = SI

End Solution Parameters

Begin Conductors

! label type      node 1   node 2   parameters
100 conduction   Tin     1       1.0, 0.5, 1.0 ! k_E L_E A_E/2
101 conduction   1       2       1.0, 0.5, 1.0 ! k_E L_E A_E/2
102 conduction   20      3       2.0, 1.0, 1.0 ! k_F L_F A_F
103 conduction   3       4       2.0, 1.0, 1.0 ! k_F L_F A_F
104 conduction   40      5       3.0, 0.5, 1.0 ! k_H L_H A_H/2
105 conduction   5       Tout    3.0, 0.5, 1.0 ! k_H L_H A_H/2

106 conduction   1       7       1.0, 1.0, 1.0 ! k_E
107 conduction   3       6       2.0, 0.5, 2.0 ! k_F
108 conduction   5       11      3.0, 1.0, 1.0 ! k_H
109 conduction   60      9       2.0, 0.5, 2.0 ! k_G

110 conduction   Tin     7       1.0, 0.5, 1.0 ! k_E L_E A_E/2
111 conduction   7       8       1.0, 0.5, 1.0 ! k_E L_E A_E/2
112 conduction   80      9       2.0, 1.0, 1.0 ! k_G L_G A_G
113 conduction   9       10      2.0, 1.0, 1.0 ! k_G L_G A_G
114 conduction   90      11      3.0, 0.5, 1.0 ! k_H L_H A_H/2
115 conduction   11      Tout    3.0, 0.5, 1.0 ! k_H L_H A_H/2

200 convection   2       20      0.1 1.0 ! h contact resistance
201 convection   4       40      0.1 1.0 ! h contact resistance
202 convection   6       60      0.1 2.0 ! h contact resistance
203 convection   8       80      0.1 1.0 ! h contact resistance
204 convection   10      90      0.1 1.0 ! h contact resistance

End Conductors

Begin Boundary Conditions

! type parameter(s) node(s)
fixed_T    1.0      Tin     ! inner wall temperature
fixed_T    0.0      Tout    ! outer wall temperature

End Boundary Conditions
```

TNSolver Output for $k_G = 2.0$

Composite Wall Model 3 with Contact Resistance

Nodes

Label	Material	Volume (m ³)	Temperature (C)
Tin	N/A	0	1
1	N/A	0	0.977612
2	N/A	0	0.955224
20	N/A	0	0.507463
3	N/A	0	0.485075
4	N/A	0	0.462687
40	N/A	0	0.0149254
5	N/A	0	0.00746269
Tout	N/A	0	1.13687e-013
7	N/A	0	0.977612
6	N/A	0	0.485075
11	N/A	0	0.00746269
60	N/A	0	0.485075
9	N/A	0	0.485075
8	N/A	0	0.955224
80	N/A	0	0.507463
10	N/A	0	0.462687
90	N/A	0	0.0149254

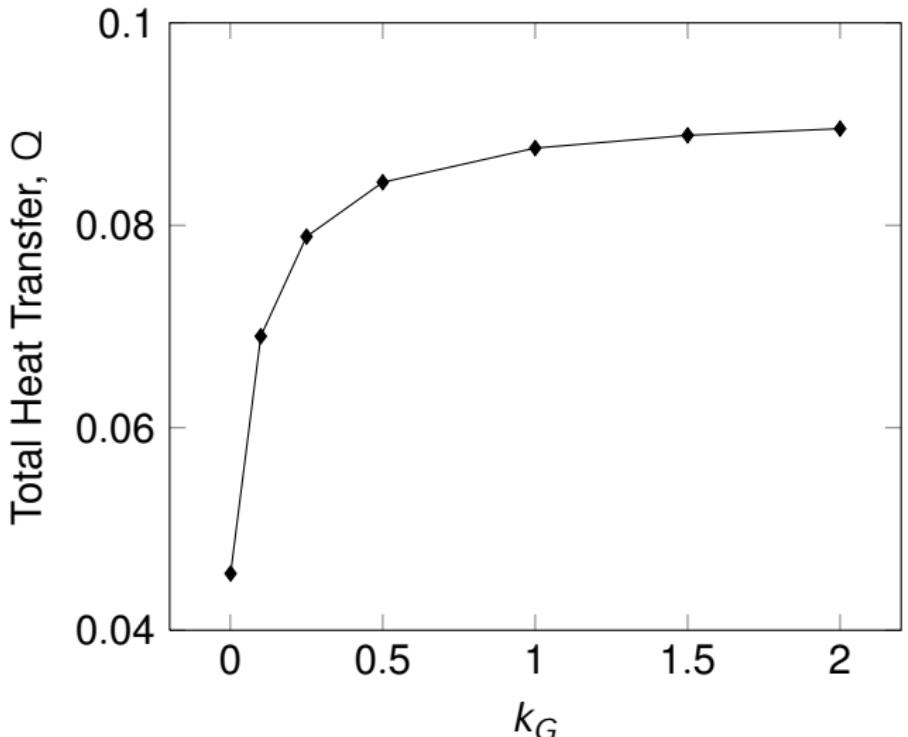
Conductors

Label	Type	Node i	Node j	$Q_{i,j}$ (W)
100	conduction	Tin	1	0.0447761
101	conduction	1	2	0.0447761
102	conduction	20	3	0.0447761
103	conduction	3	4	0.0447761
104	conduction	40	5	0.0447761
105	conduction	5	Tout	0.0447761
106	conduction	1	7	0
107	conduction	3	6	-4.54747e-013
108	conduction	5	11	0
109	conduction	60	9	0
110	conduction	Tin	7	0.0447761
111	conduction	7	8	0.0447761
112	conduction	80	9	0.0447761
113	conduction	9	10	0.0447761
114	conduction	90	11	0.0447761
115	conduction	11	Tout	0.0447761
200	convection	2	20	0.0447761
201	convection	4	40	0.0447761
202	convection	6	60	5.68434e-014
203	convection	8	80	0.0447761
204	convection	10	90	0.0447761

Total Heat Transfer over the Range of k_G

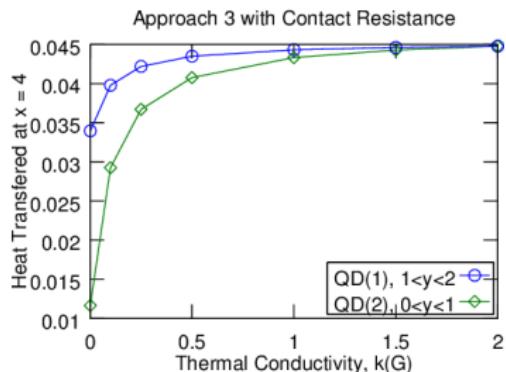
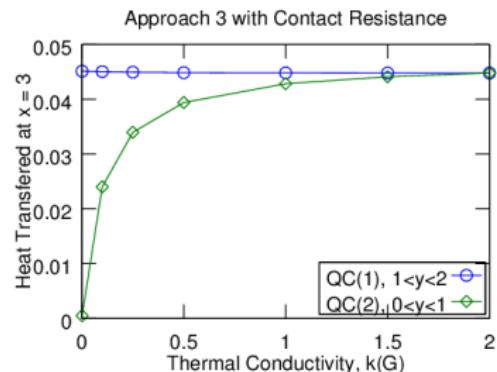
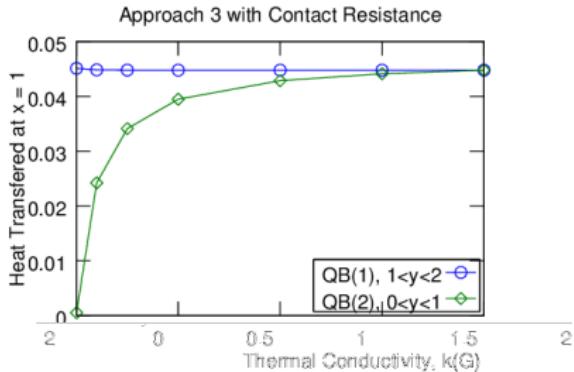
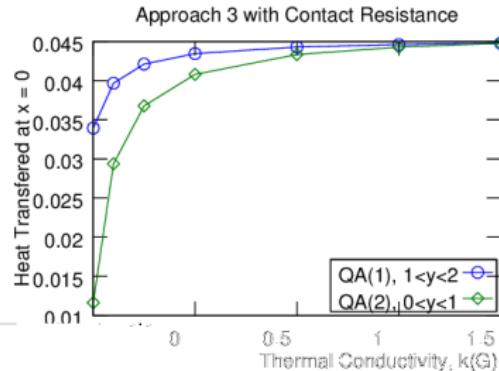
Composite Wall Model 3 with Contact Resistance

Composite Wall, 3 with Contact Resistance



Total Heat Transfer at Region Interfaces

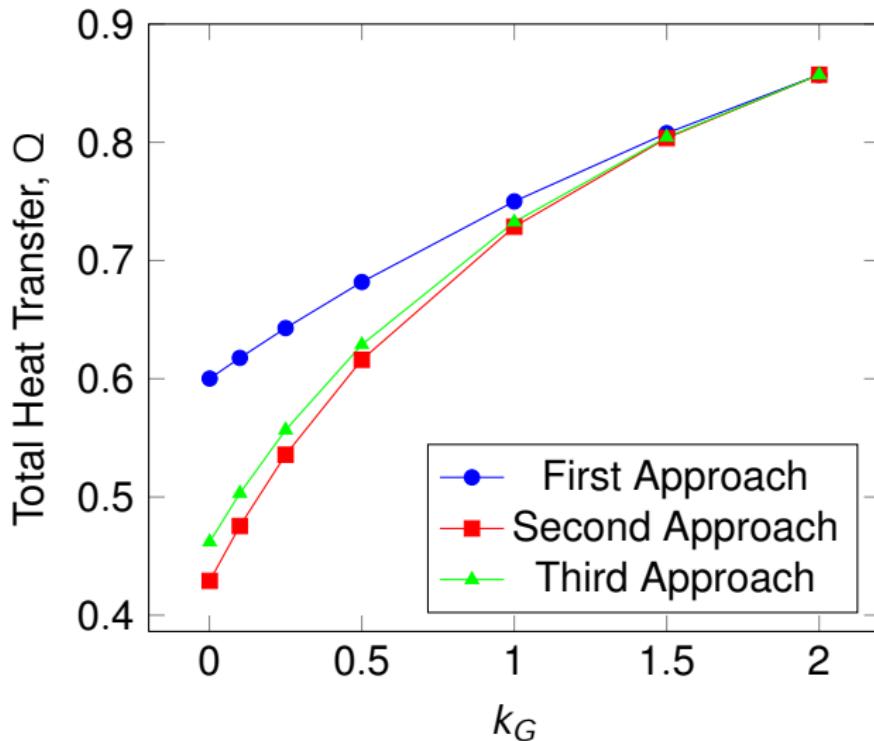
Composite Wall Model 3 with Contact Resistance



Total Heat Transfer over the Range of k_G

Composite Wall Model Summary

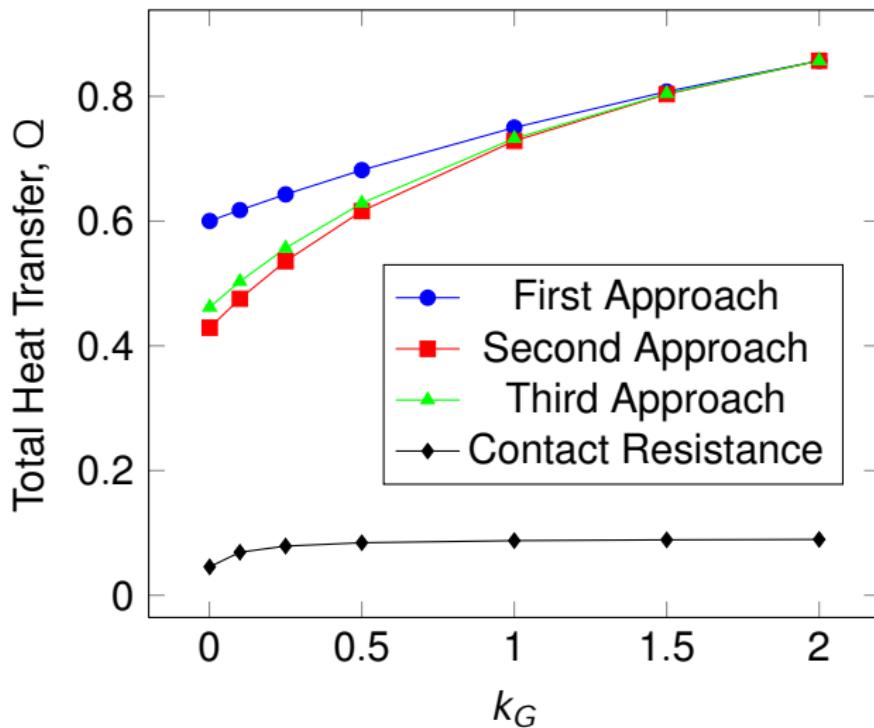
Summary of Approaches



Total Heat Transfer over the Range of k_G

Composite Wall Model Summary

Summary of Approaches



Conclusion

Questions?

Obtaining GNU Octave

GNU Octave

- ▶ **GNU Octave**
 - | <http://www.gnu.org/software/octave/>
- ▶ **Octave Wiki**
 - | <http://wiki.octave.org>
- ▶ **Octave-Forge Packages (similar to MATLAB Toolbox packages)**
 - | <http://octave.sourceforge.net>
- ▶ **For Windows installation I would suggest the MinGW installation.**
 - | If you already have Cygwin installed, then install that version.

SI Units

Quantity	Symbol	Fundamental	Derivatives
Mass	m	M	kg
Length	x, y, z	L	m
Area	A	L^2	m^2
Volume	V	L^3	m^3
Time	t	t	s
Force	F	$\frac{M \cdot L}{t^2}$	newton (N)
Energy	E	$\frac{M \cdot L^2}{t^2}$	joule (J), $N \cdot m$
Power	P	$\frac{M \cdot L^2}{t^3}$	watt (W), $\frac{J}{s}$
Rate of heat transfer	$Q = qA$	$\frac{M \cdot L^2}{t^3}$	watt (W), $\frac{J}{s}$
Heat flux	q	$\frac{M}{t^3}$	$\frac{W}{m^2}, \frac{J}{s \cdot m^2}$
Heat generation rate per unit volume	\dot{q}	$\frac{M}{L \cdot t^3}$	$\frac{W}{m^3}, \frac{J}{s \cdot m^3}$
Temperature	T	T	$^\circ C = K - 273.15$
Pressure	P	$\frac{M}{L \cdot t^2}$	pascal (Pa), $\frac{N}{m^2}$
Velocity	u, v, w	$\frac{L}{t}$	
Density	ρ	$\frac{M}{L^3}$	
Thermal conductivity	k	$\frac{M \cdot L}{t^3 \cdot T}$	$\frac{W}{m \cdot K}$
Specific heat	c	$\frac{L^2}{t^2 \cdot T}$	$\frac{J}{kg \cdot K}$
Dynamic (absolute) viscosity	μ	$\frac{M}{L \cdot t}$	$Pa \cdot s, \frac{N \cdot s}{m^2}$
Thermal diffusivity	$\alpha = \frac{k}{\rho c}$	$\frac{L^2}{t}$	
Kinematic Viscosity	$\nu = \frac{\mu}{\rho}$	$\frac{L^2}{t}$	
Convective heat transfer coefficient	h	$\frac{M}{t^3 \cdot T}$	$\frac{W}{m^2 \cdot K}, \frac{J}{s \cdot m^2 \cdot K}$

US Customary Units

Quantity	Symbol	Fundamental	Derivatives
Mass	m	M	lb_m
Length	x, y, z	L	ft
Area	A	L^2	ft^2
Volume	V	L^3	ft^3
Time	t	t	s
Force	F	$\frac{M \cdot L}{t^2}$	lb_f
Energy	E	$\frac{M \cdot L^2}{t^2}$	Btu
Power	P	$\frac{M \cdot L^2}{t^3}$	hp
Rate of heat transfer	$Q = qA$	$\frac{M \cdot L^2}{t^3}$	$\frac{Btu}{s}$
Heat flux	q	$\frac{M}{t^3}$	$\frac{Btu}{s}$
Heat generation rate per unit volume	\dot{q}	$\frac{M}{L \cdot t^3}$	$\frac{s \cdot ft^2}{s \cdot ft^3}$
Temperature	T	T	${}^\circ F = {}^\circ R - 459.67$
Pressure	P	$\frac{M}{L \cdot t^2}$	$\frac{lb_m}{ft \cdot s^2}$
Velocity	u, v, w	$\frac{L}{t}$	$\frac{ft}{s}$
Density	ρ	$\frac{M}{t^3}$	$\frac{lb_m}{ft^3}$
Thermal conductivity	k	$\frac{M \cdot L}{t^3 \cdot T}$	$\frac{Btu}{s \cdot ft \cdot R}$
Specific heat	c	$\frac{L^2 \cdot T}{M \cdot R}$	$\frac{Btu}{lb_m \cdot R}$
Dynamic (absolute) viscosity	μ	$\frac{M}{L \cdot t}$	$\frac{lb_m}{ft \cdot s}$
Thermal diffusivity	$\alpha = \frac{k}{\rho c}$	$\frac{L^2}{t}$	$\frac{ft^2}{s}$
Kinematic Viscosity	$\nu = \frac{\mu}{\rho}$	$\frac{L^2}{t}$	$\frac{ft^2}{s}$
Convective heat transfer coefficient	h	$\frac{M}{t^3 \cdot T}$	$\frac{Btu}{s \cdot ft^2 \cdot R}$

Cartesian Tensor Notation (Einstein Convention)

Cartesian tensor notation is a compact method for writing equations. A few simple rules can be used to expand an equation into its full form based on the subscript indices. The range of the indices are based on the spatial dimension of the problem. If an index is repeated within a term of the equation, then a summation over the index is implied.

Two-dimensions:

$$q_i n_i = q_1 n_1 + q_2 n_2 = q_x n_x + q_y n_y$$

Three-dimensions:

$$q_i n_i = q_1 n_1 + q_2 n_2 + q_3 n_3 = q_x n_x + q_y n_y + q_z n_z$$

References I

- [BLID11] T.L. Bergman, A.S. Lavine, F.P. Incropera, and D.P. DeWitt.
Introduction to Heat Transfer.
John Wiley & Sons, New York, sixth edition, 2011.
- [LL12] J. H. Lienhard, IV and J. H. Lienhard, V.
A Heat Transfer Textbook.
Phlogiston Press, Cambridge, Massachusetts, fourth
edition, 2012.
Available at: <http://ahtt.mit.edu>.